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Although calibration usually improves the accuracy of the measurement, it is clear that the sources of inaccuracy mentioned above still persist after the calibration and will still adversely affect the wavelength accuracy. Another disadvantage, of course, results from the additional effort that has to be spent for the calibration process.

25 According to the invention, a wavelength-determining unit for determining the
wavelengths of a plurality of successive optical signals comprises a

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wavemeter unit, an absolute-measuring unit having unambiguous wavelength properties at known absolute wavelength values, and an evaluation unit. The wavemeter unit determines (e.g. successive) wavelength values for the optical signals. The absolute-measuring unit determines such of the known absolute wavelength values covered by the optical signals. Both devices – the
5 wavemeter and the absolute measuring unit – receive the same optical signals and run substantially simultaneously.

The evaluation unit receives the determined wavelength values from the wavemeter unit and the covered known absolute wavelength values from the
10 absolute-measuring unit. The evaluation unit compares the determined wavelength values from the wavemeter with the covered known absolute wavelength values, and corrects the determined wavelength values based on the covered known absolute wavelength values.

Thus, the invention provides a correction or adjustment of the measuring
15 results that is suitable to provide an online correction. Such simultaneous calibration of wavelength values provides strong improvements in comparison to single factory site calibrations, which cannot cover individual conditions of the setup and environment during measurement. This is in particular useful when the measurement setup, in particular the wavemeter unit, is susceptible
20 for variations, e.g. by thermal or mechanical influences, which can affect the measuring conditions and/or accuracy.

In a preferred embodiment, the wavemeter unit has a wavelength characteristic known in principle or derived from former measurements. In that case, the evaluation unit adjusts the known wavelength characteristic based
25 on the covered known absolute wavelength values, and corrects the determined wavelength values accordingly.

The correction of the determined wavelength values or the wavelength characteristics of the wavemeter is preferably accomplished by correlating the covered known absolute wavelength values with determined wavelength

values or with the wavelength characteristics of the wavemeter unit, e.g. by comparing the covered known absolute wavelength value with the wavelength values determined by the wavemeter unit for the same optical signal. The evaluation unit can then determine one or more offset and/or corrections values for correcting the determined wavelength values or for calibrating the wavelength characteristics of the wavemeter unit.

The absolute-measuring unit makes use of unambiguous wavelength properties like absolutely known transmission features as provided e.g. by gas absorption cells. In such gas absorption cells, the incoming light is passed through a gas cell acting as an optical filter having known absorption lines of the gas as absolutely known transmission features. Such filters are described e.g. in US-A-5,780,843 for controlling high accuracy tunable laser sources.

A preferred embodiment of the wavemeter unit makes use of the interferometric principle, such as the Fizeau, Michelson or Fabry-Perot interferometer or uses e.g. a combination of different etalons (which can be also realized based on polarization effects) as disclosed in detail in the aforementioned EP-A- 875743. Those interferometric units generally provide a periodic dependency over the wavelength, but exhibit a higher resolution than the units employing wavelengths dependent material properties.

For providing the wavelength correction of the invention, the optical signals are swept over a wavelength range wherein the absolute-measuring unit has at least one of the known absolute wavelength characteristics. By analyzing the measured transmitted power of the absolute-measuring unit together with the wavelength-results derived from the wavemeter unit, a relation between the absolutely known transmission features and the derived wavelength-results can be established. This can result for example in one or more correction values (offset, polynomial coefficients) relating to an e.g. factory based calibration of the wavemeter unit. Because this online

calibration reflects the instantaneous measurement conditions it is more accurate than a timely and geographically separated factory based calibration could ever be.

In another embodiment, a separate wavelength source is employed providing optical signals out of the sweep band. The interference path difference in an interferometer of the wavemeter can thus be measured or controlled. This, however, is not applicable for dispersion drift and a very frequency stable source is needed.

The invention can be partly or entirely embodied by one or more suitable software programs, which can be stored on or otherwise provided by any kind of data carrier, and which might be executed in or by any suitable data processing unit. In particular, software programs might be applied by the evaluation unit and for controlling a wavelength sweep of a light source.

BRIEF DESCRIPTION OF THE DRAWINGS

Other objects and many of the attendant advantages of the present invention will be readily appreciated and become better understood by reference to the following detailed description when considering in connection with the accompanied drawings. Features that are substantially or functionally equal or similar will be referred to with the same reference sign(s).

Figure 1 shows a principle arrangement according to the invention.

Figure 2 shows a preferred embodiment according to the invention.

DETAILED DESCRIPTION OF THE INVENTION

In Fig. 1, a wavelength variable laser source 10 provides an optical signal $\lambda(t)$ having a wavelength variation over the time. The exact variation of the wavelength over time has to be determined. The optical signal $\lambda(t)$ is coupled to a wavelength-determining unit 20 comprising a wavemeter unit 30, an absolute-measuring unit 40 having unambiguous wavelength properties at

known absolute wavelength values, and an evaluation unit 50. The
wavemeter unit 30 determines wavelength values $\lambda_1(t)$ for the optical signal
 $\lambda(t)$. The absolute-measuring unit 40 determines such of the known absolute
wavelength values $\lambda_2(t)$ covered by the optical signal $\lambda(t)$. The evaluation unit
5 50 receives the determined wavelength values $\lambda_1(t)$ from the wavemeter unit
30 and the covered known absolute wavelength values $\lambda_2(t)$ from the
absolute-measuring unit 40. The evaluation unit 50 compares the determined
values of $\lambda_1(t)$ with the covered known absolute wavelength values $\lambda_2(t)$, and
provides corrected wavelength values $\lambda_1'(t)$ for determined values of $\lambda_1(t)$
10 based on the covered known absolute wavelength values $\lambda_2(t)$.

If the known absolute wavelength characteristic is provided i.e. by a gas cell,
covered absorption peaks marked by an index i lead to discrete absolute
wavelength values λ_2 at the sweep times t_i . Deviations of the relative
wavemeter values λ_1 from the absolute peak values λ_2 at the same point in
15 time describe a wavelength error $\Delta\lambda(t_i) = \lambda_1(t_i) - \lambda_2(t_i)$. The discrete function
 $\Delta\lambda$ can be inter- and extra-polated by a polynomial regression of order one or
higher giving a steady function $\Delta\lambda(t)$.

The desired calibrated wavelength λ_1' as a function of the sweep time t can
be unveiled by a subtraction of the wavelength error $\Delta\lambda(t)$ from the
20 wavelength values $\lambda_1(t)$: $\lambda_1'(t) = \lambda_1(t) - \Delta\lambda(t)$. In this way the fine structure of
the sweep signal relatively determined by the wavemeter is calibrated by the
discretely known absolute wavelength reference. If a second order
polynomial fit is deployed for the inter- and extrapolation of $\Delta\lambda(t_i)$ the typical
dispersion influence of the fiber material of the wavemeter is eliminated.
25 These calculations are part of the evaluation unit 50.

Fig. 2 shows a preferred embodiment according to the invention for testing an
optical component 100 with a swept tunable laser (TLS) 10 and a receiver 110
receiving a signal response of the optical component 100 on the stimulus
signal provided by the TLS 10. A coupler 120 provides the optical signal $\lambda(t)$

of the TLS 10 to a Michelson Fiber Interferometer (MFI) 130 with two delay lines. The mixing product is phase-shifted and detected by detectors 140 and 150, thus enabling direction-sensitive tracking.

At the detector 140 the wavelength dependent signal described by the well-known interferogram equation is observed. An additional phase-shifted detector 150 might be used to enable direction-sensitive tracking. Insofar, the MFI 130 represents the wavemeter unit 30. Both interferometric arms have to be protected against environmental disturbances (mainly vibrations) causing systematical and statistical phase fluctuations ending up in a reduced relative and absolute wavelength accuracy.

A third port of the MFI 130 is used for absolute wavelength determination, thus representing the absolute-measuring unit 40. To achieve this an absolute wavelength reference with defined absorption lines is used to generate a wavelength dependent Trace Signal at a detector 160.

It has been shown that the interference signal of the MFI 130 and therefore the wavelength information is affected by systematical and statistical phase fluctuations in the interferometer paths. Root causes include acousto-optic or temperature sensitive propagation constant drift, stress relaxation. These effects affect the relative and the absolute wavelength accuracy.

In operation, a controller 170 receives takes the data from the detectors 110, 140, (150,) and 160. From the data of the detectors 140 and 160, the wavelength values $\lambda_1'(t)$ as a function of time are evaluated in 170 (see also unit 50 in Fig. 1) and linked to the intensity values $I(t)$ of the detector 110 resulting in the spectral response $I(\lambda)$ of the optical component 100: $\lambda_1'(t)$ & $I(t) \rightarrow I(\lambda)$.

Every time when the optical signal $\lambda(t)$ sweep covers one or more absorption lines (wavelength marks) of the absolute-measuring unit 40, the controller 170 can determine an absolute wavelength offset, wavelength dependent frequency spacing of the MFI 130 (e.g. CD: 3 points), and the phase

difference of the MFI 130 at a given wavelength spacing. This can be done e.g. by using LSA fit to a reference function or determining cross-correlation.

If a counter is used, the result of the calculation of the correction value can be an error polynom with updated coefficients. This polynom can be recalculated
5 with any sweep.

If the measurement sweep does not cover wavelength marks of the absorption cell it could be extended at the cost of sweep time. This can be repeated in intervals depending on the time behavior of the phase fluctuations.

10 An evaluation unit 200 in Fig. 2 receives the signal response determined by the receiver 110 and the thereto corresponding determined wavelength values $\lambda_1'(t)$ from the controller 170.

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